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Your letter w/ manuscript  
was here when I got back yesterday  
from a week + a holiday at TRB and a consultants  
meeting in New York City.

You are dealing with Delamination. My view of  
delamination as related to concrete is not so much the  
delamination process or how did the concrete acquire a  
laminar structure i.e. where did the laminae come from  
that permitted the delamination to take place.

I looked in ACI 116R and found a definition of -  
delamination that covers a lot of ground. But 116R  
has no definition of laminae or laminar. Presumably there  
was as used in concrete technology have the same meaning  
they have in the "lay" language - ordinary speech. To  
me laminae are like pages in a book, cleavage sheets of mica  
or other layers in shale or slate. I would not call all the  
concrete about the Astropaper "delamination" etc.

Reading the 1st page of your paper it  
appears you are going to talk about honed glass  
as mentioned in 116R. Maybe you should put  
glass in the title. You say "glass" and slabs.  
All glass are slabs (not all slabs are glass). Maybe  
you mean "glass" and other slabs (like  
sidewalks?) or pavements? -

When air-entraining agent was new - and only obtained

by air-entraining cement - our lab got the task of explaining the surface scaling ("delamination" guess) that had happened w/ air-entraining cement was directly substituted for non-air-entraining cement and the water volume and slump both increased. Hence for standard placing + finishing, the coarse aggregate sank and a layer of laminated cement paste formed on top which then scaled in freezing and thawing. We called it "manipulation scaling" - i.e. the concrete got more manipulation in consolidation and finishing than it should have had.

In the last year or so I've heard a lot about coarse aggregate particles settling up after hard honing of concrete floors with entrained air - so entrained air is now forbidden in hard finished floors when all that was needed was a little more water to sink the rocks a little lower so when honed they don't bounce back up due to the compression + decompression of the air in the concrete as the honed passes down on the concrete. My comments on this have been published (I think in concrete construction).

A million metres square of airfield apron at Rastatt Germany showed severe paper thin cement paste scaling due to freezing of water in low places due to over finishing of air-entrained concrete with which the Germans were very familiar. It all happened the first winter after construction. The USAF are paranoid about small flakes and fragments - they believe, incorrectly, that these get sucked up jet engines and do damage. Not so. I shall now read the manuscript and comment.

Only "Revised"? I do not feel a reprint by you of a previous visit, so why not "State of the Art" or "Review of Knowledge"?



(2) I don't think very many faults are "labeled" at floor delamination.

(3) A floor is a slab

(4) Spalling & scaling are different hence a common is needed - as in all cases of arsenic with "and" or "or"

(5) When a unit of measure is preceded by a numeral, the unit is identified by an abbreviation or symbol "6 in," NOT "6 inches"

(6) Do not give titles of references in the text

(7) As I have written elsewhere we know that air in concrete is compressible - the pressure method for air content uses this fact; hence under heavy tamping the air is compressed the concrete runs down & bounces back up when the trowel moves on ... all this means is the concrete needs to be a little stiffer - less compressible when heavily tamped w/ air entrained. This also applies to concrete aggregate particles near the surface that get pushed down on job - pour troweling, and bounce back up & stick out of the finished surface or pull out and roll around and make trouble.

(8) I don't get the allusion in "bleeding gum effect" which is troweling like chewing gum?

(9) Bleeding stops only when solids no longer move down (sink) in the water suspension - either because they've dropped as far as they can go or (more likely) because of imbedding setting of cement that changes the water suspension to a rigid framework.

(10) Regarding the frost susceptibility of the densified non-air-entrained concrete - if it has no freezeable water and is dense and homogeneous it needs no entrained air (like a non porous rock) but if it is laminated (layered) and water can get into between the laminae (as in a slab or block) it will delaminate - what has nothing to do with whether or not it is air entrained.

(11) I do not see the need for air drying of concrete that has a proper air-void system, frost resistant aggregate, and a strength of 4000 psi - it should be immune to freezing and thawing even when critically saturated. Our lab f & t data seems to confirm this. Drying before freezing of non-frost resistant concrete will protect it by avoiding freezing while critically saturated.

(12) There is NO such thing as a water void (analogous to an air void) in concrete paste i.e. a volume of water surrounded by paste - but a quantity will simply be a zone of high w/cm paste, the only discrete volume of water in unhardened concrete bleed water voids beneath aggregate particles or other embedded items that do not sink during bleeding.

(13) I don't see how elevated air temp over the slab can increase bleeding - it will ~~increase~~ <sup>accelerate</sup> hydration i.e. so do a setting time which terminates bleeding sooner than it would otherwise stop. I also cannot understand how the relative humidity in wind across the slab can increase the loss of quantity causing solids to sink in the

fresh concrete i.e. increase bleeding rate. It will increase the rate at which blood water evaporates but not the rate at which it is produced.

(14) The term "premature stiffening" see ACI 116R means fresh setting or false setting of portland cement due to insufficient gypsum or partly dehydrated gypsum - and should not be used to mean early time of setting in general.

(15) How do you get an abnormal amount of unhydrated cement and a higher than normal amount of capillary pores since the source of water to hydrate cement is in the capillary pores. You would only get this combination if the water evaporated not only from bleeding but also from the capillary pores - which doesn't usually happen until a day or so after finishing even in dry hot weather. The internal RH has to drop to 80% or less for water to become unavailable to hydrate cement by emptying the capillary pores.

I believe the rest of my comments are clear on the marked copy.

This is an exhaustive study. It tells me - and, I'm afraid, most people more than they really want to know about delamination but it should be published for the record.

The to me unresolved question is whether you can hard machine finish a properly proportioned air-entrained concrete floor if you wait until initial setting of the concrete has not only stopped bleeding but also reduced the compressibility of the concrete (due to the air) so it doesn't feed down & bounce back under the finishing and pump up RH to make a lamellar layer. I suspect you can but I think you want till the heel joint only goes in 1/8 in or so! -

I was glad to get to read this. I learned a lot - I think you have a few bits to learn too and I hope my comments will help.

Best wishes to Berne:

John

Encl 116R 2 pp.

Richard Hester

marked copy